

EPER ELECTRIC POWER RESEARCH INSTITUTE

Multi-facet Approach for Evaluating Criticality Risks during Transportation of Commercial Spent Nuclear Fuel

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Topics

Introduction

Probability of Criticality Event during Transportation Misloading

Impact on nuclear reactivity

Under-burned fuel

Fresh fuel

Fuel Reconfiguration

Impact on nuclear reactivity

Best-estimate fuel damage assessment

Recap

Conclusion



Introduction



Storage of Nuclear Fuel No burnup restriction

Transportation of Nuclear Fuel

Restricted for burnup >45 GWd/MTU

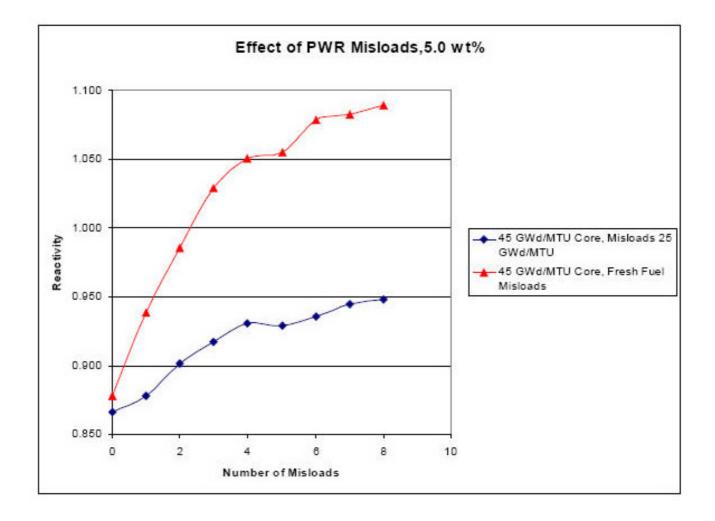
Train Container and Transport Car



Probability of Criticality Event during Rail Transportation

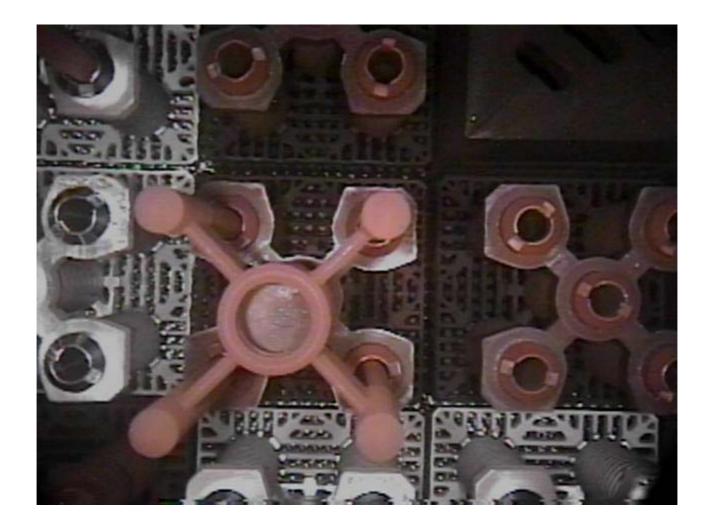
Description	Freight Trains
Train Accidents per Train-Mile (All Accidents, All Speeds, All Track Classes), 2000 - May 2006.	2.7E-06
Probability of Accident of Interest, Given Any Accident (>2% Strain and Immersion) per Modal Study	7.8E-09
Frequency of Accidents of Interest for Criticality/Train-Mile	2.1E-14
Assumed Average Number of Miles per Shipment	2,000
Frequency of Accidents of Interest for Criticality/Shipment	4.2E-11
Likelihood of Shipping a Misloaded Spent Fuel Cask	2.6E-06
Likelihood of an Accident with a Potential for Criticality/Shipment	1.1E-16

Misloading of Under-burned and Fresh Fuel – Impact on Nuclear Reactivity (Cask k_{eff})





Misloading – Fresh versus Once-burned Assemblies





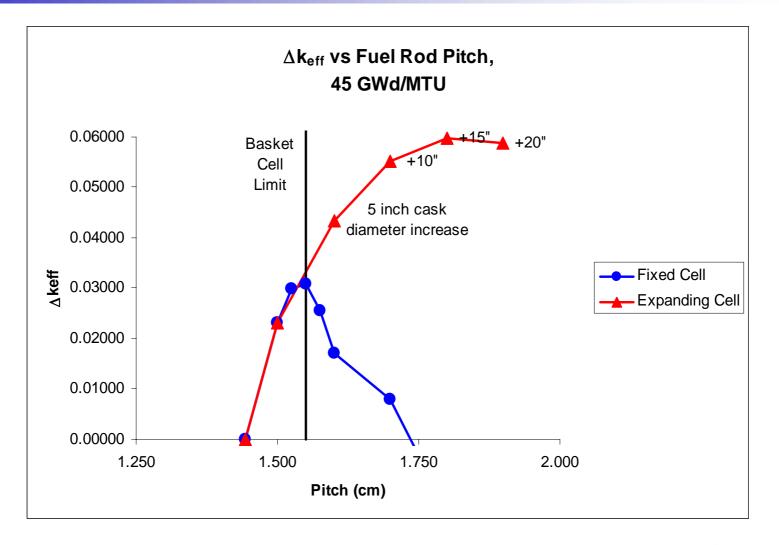
Fuel Reconfiguration – Worst Case Scenarios NUREG/CR-6835 (September 2003)

Table 6: Maximum increase in k_{eff} for each fuel failure scenario*

Scenario	MPC-24	GBC-32	MPC-68
	<u>(fresh fuel)</u>	(45 GWd/MTU)	<u>(fresh fuel)</u>
Single missing rod	. 001	<0.0010	6 003
Multiple missing rod	0140	0.0130	00120
Cladding removed from all fuel rods	0.9468	0.0349	0.0+41
Fuel rubble (no cladding)	0.063	0.0233	0.149
Assembly slips 20 cm above or			
below neutron poison panels	0001	0.0435	0.0362
Variation in pitch (without cladding)	9.070	Not calculated	0.1225

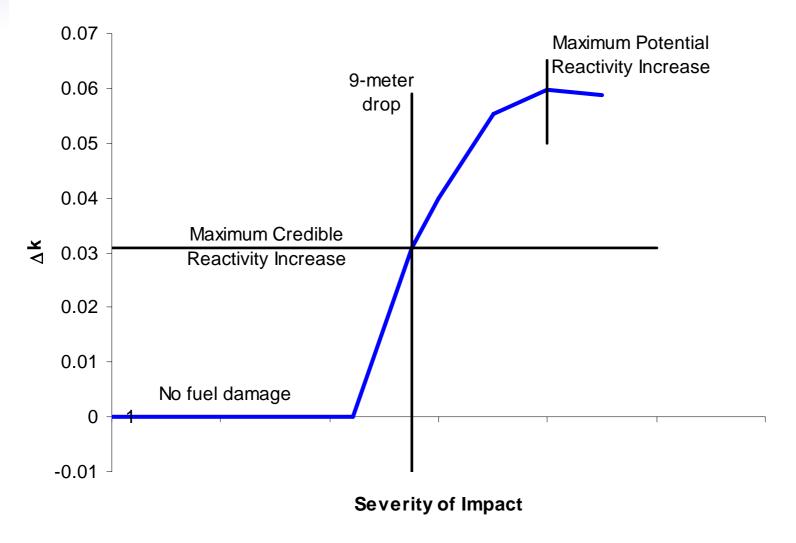
* "Although the scenarios considered go beyond credible conditions, they represent a theoretical limit on the effects of severe accident conditions" (NUREG/CR-6835, p. 1)

Fuel Reconfiguration – Worst Case Scenarios



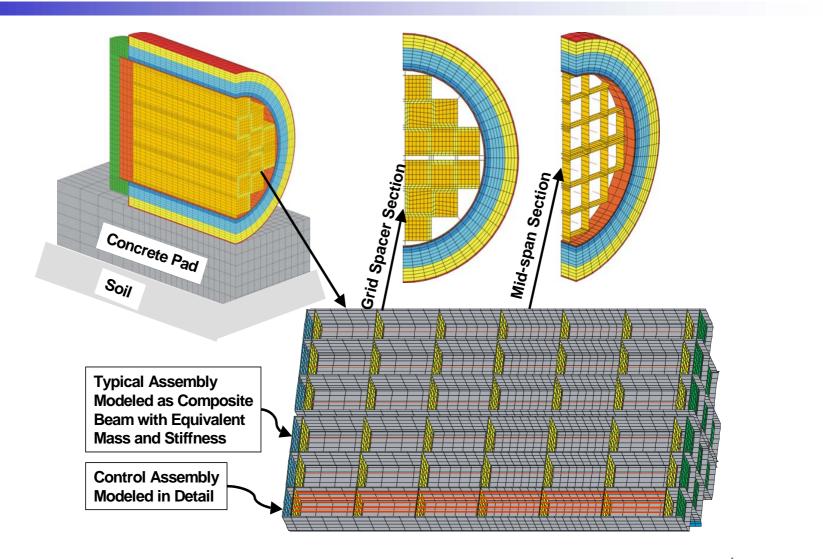


Fuel Reconfiguration – Worst Case Scenarios



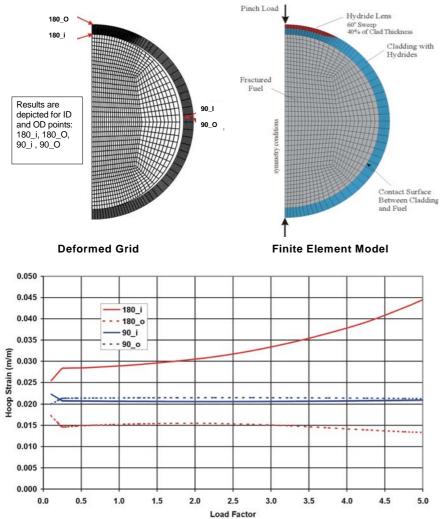


Fuel Damage Evaluation – Best-Estimate Approach





Fuel Damage Evaluation – Best-Estimate Approach



- The fuel column, as an integral part of high-burnup spent fuel rods, plays the primary role in limiting cladding stresses
- The fuel-cladding gap is found to be the major protagonist for failure initiation that has the potential to propagate to through-wall fracture
- Using highly conservative assumptions on the role of the gap in inducing through-wall failure → through-wall failure probability: ~1E-5/rod



Recap

- Normal configuration of cask contents: $k_{eff} < 0.95$
- Probability of criticality event during rail transportation accident: ~10⁻¹⁶/shipment
 - Probability of accident
 - Conditional probability associated with accident severity and intrusion of moderator
 - Probability of one misloaded assembly in the cask
- Conservatisms
 - Multiple misloadings of severely under-burned or fresh fuel
 - Administrative controls (dedicated trains)
- Fuel relocation
 - Cannot rule out small increases in k_{eff} , but increases in k_{eff} are unlikely and less than safety margin
 - Best-estimate analyses show limited assembly damage



Conclusion

- No credible combination of rail transportation accident events and fuel misloading or reconfiguration can result in a critical configuration
- Overall transportation risks include non-radiological risks that are directly proportional to the number of shipments
 - Misallocation of regulatory requirements associated by radiological risks can lead to greater overall risks by overly restricting payloads
- High-capacity rail casks represent the lowest risk for transporting commercial spent nuclear fuel, regardless of the enrichment or burnup of the fuel

